

ISSN 2518-170X (Online)

ISSN 2224-5278 (Print)



ҚАЙЫРЫМДЫЛЫҚ ҚОРЫ

HALYK

CHARITY FOUNDATION

«ҚАЗАҚСТАН РЕСПУБЛИКАСЫ
ҰЛТТЫҚ ҒЫЛЫМ АКАДЕМИЯСЫ» РҚБ
«ХАЛЫҚ» ЖҚ

Х А Б А Р Л А Р Ы

ИЗВЕСТИЯ

РОО «НАЦИОНАЛЬНОЙ
АКАДЕМИИ НАУК РЕСПУБЛИКИ
КАЗАХСТАН»
ЧФ «Халық»

N E W S

OF THE ACADEMY OF SCIENCES
OF THE REPUBLIC OF
KAZAKHSTAN
«Halyk» Private Foundation

SERIES

OF GEOLOGY AND TECHNICAL SCIENCES

1 (463)

JANUARY – FEBRUARY 2024

THE JOURNAL WAS FOUNDED IN 1940

PUBLISHED 6 TIMES A YEAR

ALMATY, NAS RK

NAS RK is pleased to announce that News of NAS RK. Series of geology and technical sciences scientific journal has been accepted for indexing in the Emerging Sources Citation Index, a new edition of Web of Science. Content in this index is under consideration by Clarivate Analytics to be accepted in the Science Citation Index Expanded, the Social Sciences Citation Index, and the Arts & Humanities Citation Index. The quality and depth of content Web of Science offers to researchers, authors, publishers, and institutions sets it apart from other research databases. The inclusion of News of NAS RK. Series of geology and technical sciences in the Emerging Sources Citation Index demonstrates our dedication to providing the most relevant and influential content of geology and engineering sciences to our community.

Қазақстан Республикасы Ұлттық ғылым академиясы «ҚР ҰҒА Хабарлары. Геология және техникалық ғылымдар сериясы» ғылыми журналының Web of Science-тің жаңаланған нұсқасы Emerging Sources Citation Index-те индекстелуге қабылданғанын хабарлайды. Бұл индекстелу барысында Clarivate Analytics компаниясы журналды одан әрі the Science Citation Index Expanded, the Social Sciences Citation Index және the Arts & Humanities Citation Index-ке қабылдау мәселесін қарастыруда. Web of Science зерттеушілер, авторлар, баспашылар мен мекемелерге контент тереңдігі мен сапасын ұсынады. ҚР ҰҒА Хабарлары. Геология және техникалық ғылымдар сериясы Emerging Sources Citation Index-ке енуі біздің қоғамдастық үшін ең өзекті және беделді геология және техникалық ғылымдар бойынша контентке адалдығымызды білдіреді.

НАНПК сообщает, что научный журнал «Известия НАНПК. Серия геологии и технических наук» был принят для индексирования в Emerging Sources Citation Index, обновленной версии Web of Science. Содержание в этом индексировании находится в стадии рассмотрения компанией Clarivate Analytics для дальнейшего принятия журнала в the Science Citation Index Expanded, the Social Sciences Citation Index и the Arts & Humanities Citation Index. Web of Science предлагает качество и глубину контента для исследователей, авторов, издателей и учреждений. Включение Известия НАНПК. Серия геологии и технических наук в Emerging Sources Citation Index демонстрирует нашу приверженность к наиболее актуальному и влиятельному контенту по геологии и техническим наукам для нашего сообщества.



ЧФ «ХАЛЫҚ»

В 2016 году для развития и улучшения качества жизни казахстанцев был создан частный Благотворительный фонд «Халык». За годы своей деятельности на реализацию благотворительных проектов в областях образования и науки, социальной защиты, культуры, здравоохранения и спорта, Фонд выделил более 45 миллиардов тенге.

Особое внимание Благотворительный фонд «Халык» уделяет образовательным программам, считая это направление одним из ключевых в своей деятельности. Оказывая поддержку отечественному образованию, Фонд вносит свой посильный вклад в развитие качественного образования в Казахстане. Тем самым способствуя росту числа людей, способных менять жизнь в стране к лучшему – профессионалов в различных сферах, потенциальных лидеров и «великих умов». Одной из значимых инициатив фонда «Халык» в образовательной сфере стал проект *Ozgeris powered by Halyk Fund* – первый в стране бизнес-инкубатор для учащихся 9-11 классов, который помогает развивать необходимые в современном мире предпринимательские навыки. Так, на содействие малому бизнесу школьников было выделено более 200 грантов. Для поддержки талантливых и мотивированных детей Фонд неоднократно выделял гранты на обучение в Международной школе «Мирас» и в Astana IT University, а также помог казахстанским школьникам принять участие в престижном конкурсе «USTEM Robotics» в США. Авторские работы в рамках проекта «Тәлімгер», которому Фонд оказал поддержку, легли в основу учебной программы, учебников и учебно-методических книг по предмету «Основы предпринимательства и бизнеса», преподаваемого в 10-11 классах казахстанских школ и колледжей.

Помимо помощи школьникам, учащимся колледжей и студентам Фонд считает важным внести свой вклад в повышение квалификации педагогов, совершенствование их знаний и навыков, поскольку именно они являются проводниками знаний будущих поколений казахстанцев. При поддержке Фонда «Халык» в южной столице был организован ежегодный городской конкурс педагогов «Almaty Digital Ustaz».

Важной инициативой стал реализуемый проект по обучению основам финансовой грамотности преподавателей из восьми областей Казахстана, что должно оказать существенное влияние на воспитание финансовой грамотности и предпринимательского мышления у нового поколения граждан страны.

Необходимую помощь Фонд «Халык» оказывает и тем, кто особенно остро в ней нуждается. В рамках социальной защиты населения активно проводится

работа по поддержке детей, оставшихся без родителей, детей и взрослых из социально уязвимых слоев населения, людей с ограниченными возможностями, а также обеспечению нуждающихся социальным жильем, строительству социально важных объектов, таких как детские сады, детские площадки и физкультурно-оздоровительные комплексы.

В копилку добрых дел Фонда «Халык» можно добавить оказание помощи детскому спорту, куда относится поддержка в развитии детского футбола и карате в нашей стране. Жизненно важную помощь Благотворительный фонд «Халык» оказал нашим соотечественникам во время недавней пандемии COVID-19. Тогда, в разгар тяжелой борьбы с коронавирусной инфекцией Фонд выделил свыше 11 миллиардов тенге на приобретение необходимого медицинского оборудования и дорогостоящих медицинских препаратов, автомобилей скорой медицинской помощи и средств защиты, адресную материальную помощь социально уязвимым слоям населения и денежные выплаты медицинским работникам.

В 2023 году наряду с другими проектами, нацеленными на повышение благосостояния казахстанских граждан Фонд решил уделить особое внимание науке, поскольку она является частью общественной культуры, а уровень ее развития определяет уровень развития государства.

Поддержка Фондом выпуска журналов Национальной Академии наук Республики Казахстан, которые входят в международные фонды Scopus и Wos и в которых публикуются статьи отечественных ученых, докторантов и магистрантов, а также научных сотрудников высших учебных заведений и научно-исследовательских институтов нашей страны является не менее значимым вкладом Фонда в развитие казахстанского общества.

**С уважением,
Благотворительный Фонд «Халык»!**

Бас редактор

ЖҰРЫНОВ Мұрат Жұрынұлы, химия ғылымдарының докторы, профессор, ҚР ҰҒА академигі, «Қазақстан Республикасы Ұлттық ғылым академиясы» РҚБ-нің президенті, АҚ «Д.В. Сокольский атындағы отын, катализ және электрохимия институтының» бас директоры (Алматы, Қазақстан) **Н = 4**

Ғылыми хатшы

АБСАДЫКОВ Бахыт Нарикбайұлы, техника ғылымдарының докторы, профессор, ҚР ҰҒА жауапты хатшысы, А.Б. Бектұров атындағы химия ғылымдары институты (Алматы, Қазақстан) **Н = 5**

Редакциялық алқа:

ӘБСАМЕТОВ Мәліс Құдысұлы (бас редактордың орынбасары), геология-минералогия ғылымдарының докторы, профессор, ҚР ҰҒА академигі, «У.М. Ахмедсафина атындағы гидрогеология және геоэкология институтының» директоры (Алматы, Қазақстан) **Н = 2**

ЖОЛТАЕВ Герой Жолтайұлы (бас редактордың орынбасары), геология-минералогия ғылымдарының докторы, профессор, Қ.И. Сатпаев атындағы геология ғылымдары институтының директоры (Алматы, Қазақстан) **Н = 2**

СНОУ Дэниел, Ph.D, қауымдастырылған профессор, Небраска университетінің Су ғылымдары зертханасының директоры (Небраска штаты, АҚШ) **Н = 32**

ЗЕЛЪТМАН Реймар, Ph.D, табиғи тарих мұражайының Жер туралы ғылымдар бөлімінде петрология және пайдалы қазбалар кен орындары саласындағы зерттеулердің жетекшісі (Лондон, Англия) **Н = 37**

ПАНФИЛОВ Михаил Борисович, техника ғылымдарының докторы, Нанси университетінің профессоры (Нанси, Франция) **Н = 15**

ШЕН Пин, Ph.D, Қытай геологиялық қоғамының тау геологиясы комитеті директорының орынбасары, Американдық экономикалық геологтар қауымдастығының мүшесі (Пекин, Қытай) **Н = 25**

ФИШЕР Аксель, Ph.D, Дрезден техникалық университетінің қауымдастырылған профессоры (Дрезден, Берлин) **Н = 6**

КОНТОРОВИЧ Алексей Эмильевич, геология-минералогия ғылымдарының докторы, профессор, РҒА академигі, А.А. Трофимука атындағы мұнай-газ геологиясы және геофизика институты (Новосибирск, Ресей) **Н = 19**

АГАБЕКОВ Владимир Енокович, химия ғылымдарының докторы, Беларусь ҰҒА академигі, Жаңа материалдар химиясы институтының құрметті директоры (Минск, Беларусь) **Н = 13**

КАТАЛИН Стефан, Ph.D, Дрезден техникалық университетінің қауымдастырылған профессоры (Дрезден, Берлин) **Н = 20**

СЕЙТМҰРАТОВА Элеонора Юсуповна, геология-минералогия ғылымдарының докторы, профессор, ҚР ҰҒА корреспондент-мүшесі, Қ.И. Сатпаев атындағы Геология ғылымдары институты зертханасының меңгерушісі (Алматы, Қазақстан) **Н = 11**

САҒЫНТАЕВ Жанай, Ph.D, қауымдастырылған профессор, Назарбаев университеті (Нұр-Сұлтан, Қазақстан) **Н = 11**

ФРАТТИНИ Паоло, Ph.D, Бикокк Милан университеті қауымдастырылған профессоры (Милан, Италия) **Н = 28**

«ҚР ҰҒА» РҚБ Хабарлары. Геология және техникалық ғылымдар сериясы».

ISSN 2518-170X (Online),

ISSN 2224-5278 (Print)

Меншіктеуші: «Қазақстан Республикасының Ұлттық ғылым академиясы» РҚБ (Алматы қ.).

Қазақстан Республикасының Ақпарат және қоғамдық даму министрлігінің Ақпарат комитетінде 29.07.2020 ж. берілген № **KZ39VPU00025420** мерзімдік басылым тіркеуіне қойылу туралы куәлік.

Тақырыптық бағыты: *геология, мұнай және газды өңдеудің химиялық технологиялары, мұнай химиясы, металдарды алу және олардың қосындыларының технологиясы.*

Мерзімділігі: жылына 6 рет.

Тиражы: 300 дана.

Редакцияның мекен-жайы: 050010, Алматы қ., Шевченко көш., 28, 219 бөл., тел.: 272-13-19

<http://www.geolog-technical.kz/index.php/en/>

© «Қазақстан Республикасының Ұлттық ғылым академиясы» РҚБ, 2024

Главный редактор

ЖУРИНОВ Мурат Журинович, доктор химических наук, профессор, академик НАН РК, президент РОО «Национальной академии наук Республики Казахстан», генеральный директор АО «Институт топлива, катализа и электрохимии им. Д.В. Сокольского» (Алматы, Казахстан) **Н = 4**

Ученый секретарь

АБСАДЫКОВ Бахыт Нарикбаевич, доктор технических наук, профессор, ответственный секретарь НАН РК, Институт химических наук им. А.Б. Бектурова (Алматы, Казахстан) **Н = 5**

Редакционная коллегия:

АБСАМЕТОВ Малис Кудысович, (заместитель главного редактора), доктор геологоминералогических наук, профессор, академик НАН РК, директор Института гидрогеологии и геоэкологии им. У.М. Ахмедсафина (Алматы, Казахстан) **Н = 2**

ЖОЛТАЕВ Герой Жолтаевич, (заместитель главного редактора), доктор геологоминералогических наук, профессор, директор Института геологических наук им. К.И. Сатпаева (Алматы, Казахстан) **Н=2**

СНОУ Дэниел, Ph.D, ассоциированный профессор, директор Лаборатории водных наук университета Небраски (штат Небраска, США) **Н = 32**

ЗЕЛЬТМАН Реймар, Ph.D, руководитель исследований в области петрологии и месторождений полезных ископаемых в Отделе наук о Земле Музея естественной истории (Лондон, Англия) **Н = 37**

ПАНФИЛОВ Михаил Борисович, доктор технических наук, профессор Университета Нанси (Нанси, Франция) **Н=15**

ШЕН Пин, Ph.D, заместитель директора Комитета по горной геологии Китайского геологического общества, член Американской ассоциации экономических геологов (Пекин, Китай) **Н = 25**

ФИШЕР Аксель, ассоциированный профессор, Ph.D, технический университет Дрезден (Дрезден, Берлин) **Н = 6**

КОНТОРОВИЧ Алексей Эмильевич, доктор геолого-минералогических наук, профессор, академик РАН, Институт нефтегазовой геологии и геофизики им. А.А. Трофимука СО РАН (Новосибирск, Россия) **Н = 19**

АГАБЕКОВ Владимир Енокович, доктор химических наук, академик НАН Беларуси, почетный директор Института химии новых материалов (Минск, Беларусь) **Н = 13**

КАТАЛИН Стефан, Ph.D, ассоциированный профессор, Технический университет (Дрезден, Берлин) **Н = 20**

СЕЙТМУРАТОВА Элеонора Юсуповна, доктор геолого-минералогических наук, профессор, член-корреспондент НАН РК, заведующая лабораторией Института геологических наук им. К.И. Сатпаева (Алматы, Казахстан) **Н=11**

САГИНТАЕВ Жанай, Ph.D, ассоциированный профессор, Назарбаев университет (Нурсултан, Казахстан) **Н = 11**

ФРАТТИНИ Паоло, Ph.D, ассоциированный профессор, Миланский университет Бикокк (Милан, Италия) **Н = 28**

«Известия РОО «НАН РК». Серия геологии и технических наук».

ISSN 2518-170X (Online),

ISSN 2224-5278 (Print)

Собственник: Республиканское общественное объединение «Национальная академия наук Республики Казахстан» (г. Алматы).

Свидетельство о постановке на учет периодического печатного издания в Комитете информации Министерства информации и общественного развития Республики Казахстан № **KZ39VPY00025420**, выданное 29.07.2020 г.

Тематическая направленность: *геология, химические технологии переработки нефти и газа, нефтехимия, технологии извлечения металлов и их соединений.*

Периодичность: 6 раз в год.

Тираж: 300 экземпляров.

Адрес редакции: 050010, г. Алматы, ул. Шевченко, 28, оф. 219, тел.: 272-13-19

<http://www.geolog-technical.kz/index.php/en/>

© РОО «Национальная академия наук Республики Казахстан», 2024

Editorial chief

ZHURINOV Murat Zhurinovich, doctor of chemistry, professor, academician of NAS RK, president of the National Academy of Sciences of the Republic of Kazakhstan, general director of JSC “Institute of fuel, catalysis and electrochemistry named after D.V. Sokolsky» (Almaty, Kazakhstan) **H = 4**

Scientific secretary

ABSADYKOV Bakhyt Narikbaevich, doctor of technical sciences, professor, executive secretary of NAS RK, Bekturov Institute of chemical sciences (Almaty, Kazakhstan) **H = 5**

Editorial board:

ABSAMETOV Malis Kudysovich, (deputy editor-in-chief), doctor of geological and mineralogical sciences, professor, academician of NAS RK, director of the Akhmedsafin Institute of hydrogeology and hydrophysics (Almaty, Kazakhstan) **H=2**

ZHOLTAEV Geroy Zholtaevich, (deputy editor-in-chief), doctor of geological and mineralogical sciences, professor, director of the institute of geological sciences named after K.I. Satpayev (Almaty, Kazakhstan) **H=2**

SNOW Daniel, Ph.D, associate professor, director of the laboratory of water sciences, Nebraska University (Nebraska, USA) **H = 32**

ZELTMAN Reyman, Ph.D, head of research department in petrology and mineral deposits in the Earth sciences section of the museum of natural history (London, England) **H = 37**

PANFILOV Mikhail Borisovich, doctor of technical sciences, professor at the Nancy University (Nancy, France) **H=15**

SHEN Ping, Ph.D, deputy director of the Committee for Mining geology of the China geological Society, Fellow of the American association of economic geologists (Beijing, China) **H = 25**

FISCHER Axel, Ph.D, associate professor, Dresden University of technology (Dresden, Germany) **H=6**

KONTOROVICH Aleksey Emilievich, doctor of geological and mineralogical sciences, professor, academician of RAS, Trofimuk Institute of petroleum geology and geophysics SB RAS (Novosibirsk, Russia) **H = 19**

AGABEKOV Vladimir Enokovich, doctor of chemistry, academician of NAS of Belarus, honorary director of the Institute of chemistry of new materials (Minsk, Belarus) **H = 13**

KATALIN Stephan, Ph.D, associate professor, Technical university (Dresden, Berlin) **H = 20**

SEITMURATOVA Eleonora Yusupovna, doctor of geological and mineralogical sciences, professor, corresponding member of NAS RK, head of the laboratory of the Institute of geological sciences named after K.I. Satpayev (Almaty, Kazakhstan) **H=11**

SAGINTAYEV Zhanay, Ph.D, associate professor, Nazarbayev University (Nursultan, Kazakhstan) **H = 11**

FRATTINI Paolo, Ph.D, associate professor, university of Milano-Bicocca (Milan, Italy) **H = 28**

News of the National Academy of Sciences of the Republic of Kazakhstan. Series of geology and technology sciences.

ISSN 2518-170X (Online),

ISSN 2224-5278 (Print)

Owner: RPA «National Academy of Sciences of the Republic of Kazakhstan» (Almaty).

The certificate of registration of a periodical printed publication in the Committee of information of the Ministry of Information and Social Development of the Republic of Kazakhstan **No. KZ39VPY00025420**, issued 29.07.2020.

Thematic scope: *geology, chemical technologies for oil and gas processing, petrochemistry, technologies for extracting metals and their connections.*

Periodicity: 6 times a year.

Circulation: 300 copies.

Editorial address: 28, Shevchenko str., of. 219, Almaty, 050010, tel. 272-13-19

<http://www.geolog-technical.kz/index.php/en/>

© National Academy of Sciences of the Republic of Kazakhstan, 2024

NEWS of the National Academy of Sciences of the Republic of Kazakhstan
SERIES OF GEOLOGY AND TECHNICAL SCIENCES
ISSN 2224–5278
Volume 1. Number 463 (2024), 201–217
<https://doi.org/10.32014/2024.2518-170X.376>

UDC 622.232

© O.S. Reshetnikova*, K.B. Kyzyrov, V.V. Yurchenko, 2024

Non-commercial Joint Stock Company «Karaganda Technical University named after
Abylkas Saginov», Karaganda, Kazakhstan.
E-mail: olga.reshetnikova.80@mail.ru

STRUCTURAL SYNTHESIS OF HYDRAULIC IMPACT MECHANISMS WITH A COMBINED CONTROL BODY

Reshetnikova O.S. — PhD, senior lecturer of the Department «Technological equipment, mechanical engineering and standardization», Non-commercial Joint Stock Company «Karaganda Technical University named after Abylkas Saginov»

E-mail olga.reshetnikova.80@mail.ru, <https://orcid.org/0000-0002-6965-4569>;

Kyzyrov K.B. — candidate of technical sciences, professor of the Department «Technological equipment, mechanical engineering and standardization», Non-commercial Joint Stock Company «Karaganda Technical University named after Abylkas Saginov»

E-mail kyzyrovkairulla@gmail.com, <https://orcid.org/0000-0001-6868-3643>;

Yurchenko V.V. — PhD, Head of the Department «Technological equipment, mechanical engineering and standardization», Non-commercial Joint Stock Company «Karaganda Technical University named after Abylkas Saginov»

E-mail juvv76@mail.ru, <https://orcid.org/0000-0002-6543-1632>.

Abstract. The article is devoted to the study and substantiation of the choice of the optimal constructive scheme of the hydraulic impact mechanism that meets the requirements of the main technological purpose - generating a given energy and frequency of impacts with the most simplified structure with a sufficiently high efficiency energy conversion. This pursues the goal of choosing the basic structure for creating domestic hydraulic impact mechanisms that are distinguished by high manufacturability, reliability, compactness and patentability. The substantiation of the choice of the optimal scheme that satisfies the requirements of the task was made using structural synthesis, using the main provisions of the method of functional structure formation, which consists in explaining and describing the object under study, in which its elements and the links between them are analyzed within the framework of a single whole. Logically consistently using the methods of combining and substituting the functions of the elements of the impact mechanism, using various combinations of kinematic and structural links between them, imposing certain restrictions on the combination of links of these elements, as well as using the idea of changing the energy level of the limited structural volume of hydraulic working chambers due to the effect of compressibility and expansion working fluid, a constructive scheme was determined

that meets the above requirements for further research. The scheme has a controlled working stroke chamber, an uncontrolled idle chamber with combined functions of the control element and using the effect of a hydraulic spring. This circuit is distinguished by the smallest number of elements and connections between them, which simplifies the design of the impact mechanism and reduces the number of transients, providing a more efficient transfer of energy to the tool.

Keywords: hydraulic impact mechanism; hydraulic perforator, structural synthesis; structure formation; structural formula

© **О.С. Решетникова***, **Қ.Б. Қызыров**, **В.В. Юрченко**, 2024

«Әбілқас Сағынов атындағы Қарағанды техникалық университеті»

Коммерциялық емес Акционерлік Қоғамы, Қарағанды, Қазақстан.

E-mail: olga.reshetnikova.80@mail.ru

БІРІКТІРІЛГЕН БАСҚАРУ ОРГАНЫМЕН ГИДРАВЛИКАЛЫҚ МҮШЕСІНІҢ МЕХАНИЗМДЕРІНІҢ ҚҰРЫЛЫМДЫҚ СИНТЕЗІ

Решетникова О.С. — PhD, «Технологиялық жабдықтары, машина жасау және стандарттау» кафедрасының аға оқытушысы, «Әбілқас Сағынов атындағы Қарағанды техникалық университеті» КЕАҚ

E-mail: olga.reshetnikova.80@mail.ru, <https://orcid.org/0000-0002-6965-4569>;

Қызыров К.Б. — т.ғ.к., «Технологиялық жабдықтары, машина жасау және стандарттау» кафедрасының профессоры «Әбілқас Сағынов атындағы Қарағанды техникалық университеті» КЕАҚ

E-mail: @gmail.com, <https://orcid.org/0000-0001-6868-3643>;

Юрченко В.В. — PhD, «Технологиялық жабдықтары, машина жасау және стандарттау» кафедрасының меңгерушісі, «Әбілқас Сағынов атындағы Қарағанды техникалық университеті» КЕАҚ

E-mail juvv76@mail.ru, <https://orcid.org/0000-0002-6543-1632>.

Аннотация. Мақала негізгі технологиялық мақсатты орындау талаптарына жауап беретін гидравликалық соққы механизмінің оңтайлы сұлбасын таңдауды зерттеуге және негіздеуге арналған – берілген энергияны генерациялау және энергияны түрлендірудің тиімділігі жоғары максималды жеңілдетілген құрылыммен соққы жиілігі. Бұл жоғары өнімділікпен, сенімділікпен және патенттілікпен ерекшеленетін отандық гидравликалық соққы механизмдерін құру үшін негізгі құрылымды таңдау мақсатын көздейді. Қойылған міндеттің талаптарын үйлесу, оңтайлы сұлбасын таңдаудың негіздемесі құрылымдық синтезді қолдана отырып, зерттелетін объектіні түсіндіру мен сипаттаудан тұратын функционалды құрылымдау әдісінің негізгі ережелерін қолдана отырып, оның элементтері мен олардың арасындағы қатынастар тұтастық шеңберінде талданады. Соққы механизмі элементтерінің функцияларын біріктіру және ауыстыру әдістерін логикалық дәйекті түрде қолданып, олардың арасындағы кинематикалық және конструктивті байланыстардың әртүрлі комбинацияларын және осы элементтердің байланыстарының тіркесіміне белгілі бір шектеулерді

койып, гидравликалық жұмыс камераларының шектеулі құрылымдық көлемінің энергетикалық деңгейін өзгерту идеясын қолдана отырып, жұмыс сұйықтығының сығылу және кеңею әсері арқылы жоғарыда аталған талаптарға жауап беретін конструктивті сұлбасы анықталды және қосымша зерттеулер үшін қолданды. Схемада басқарылатын жұмыс камерасы, басқару органының функциялары біріктірілген және гидравликалық серіппелі әсерді қолданатын басқарылмайтын бос камера бар. Бұл сұлба соққы механизмінің құрылысын жеңілдететін және өтпелі процестердің санын азайтатын, құралға энергияны тиімдірек беруді қамтамасыз ететін элементтер мен олардың арасындағы байланыстардың ең аз санымен ерекшеленеді.

Түйін сөздер: гидравликалық соққы механизмі; гидроперфоратор, құрылымдық синтез; құрылымның қалыптасуы; құрылымдық формула

© **О.С. Решетникова***, **К.Б. Кызыров**, **В.В. Юрченко**, 2024

Некоммерческое акционерное общество «Карагандинский технический университет имени Абылкаса Сагинова», Караганда, Казахстан
E-mail: olga.reshetnikova.80@mail.ru

СТРУКТУРНЫЙ СИНТЕЗ ГИДРАВЛИЧЕСКИХ УДАРНЫХ МЕХАНИЗМОВ С СОВМЕЩЕННЫМ ОРГАНОМ УПРАВЛЕНИЯ

Решетникова О.С. — PhD, старший преподаватель кафедры «Технологическое оборудование, машиностроение и стандартизация», НАО «Карагандинский технический университет имени Абылкаса Сагинова»

E-mail: reshetnikova.80@mail.ru, <https://orcid.org/0000-0002-6965-4569>;

Кызыров К.Б. — к.т.н., профессор кафедры «Технологическое оборудование, машиностроение и стандартизация», НАО «Карагандинский технический университет имени Абылкаса Сагинова»

E-mail: kyzurovkairulla@gmail.com, <https://orcid.org/0000-0001-6868-3643>;

Юрченко В.В. — PhD, заведующий кафедрой «Технологическое оборудование, машиностроение и стандартизация», НАО «Карагандинский технический университет имени Абылкаса Сагинова»

E-mail: juvv76@mail.ru, <https://orcid.org/0000-0002-6543-1632>.

Аннотация. Статья посвящена исследованию и обоснованию выбора оптимальной конструктивной схемы гидравлического ударного механизма, отвечающей требованиям выполнения основного технологического назначения – генерации заданной энергии и частоты ударов при максимально упрощенной структуре с достаточно высокой эффективностью энергопреобразования. Этим преследуется цель выбора базовой структуры для создания отечественных гидравлических ударных механизмов, отличающихся высокой технологичностью, надежностью, компактностью и патентоспособностью. Обоснование выбора оптимальной схемы, удовлетворяющей требованиям поставленной задачи произведено с применением структурного синтеза, использующего основные положения метода функционального структурообразования, заключающегося в объяснении и описании исследуемого объекта, при котором анализируются его элементы и взаимосвязи между ними в рамках единого целого. Логически

последовательно используя приемы совмещения и замещения функций элементов ударного механизма, применяя различные сочетания кинематических и конструктивных связей между ними, наложения определенных ограничений на сочетание связей этих элементов, а также используя идею изменения энергетического уровня ограниченного конструктивного объема гидравлических рабочих камер за счет эффекта сжимаемости и расширения рабочей жидкости была определена конструктивная схема, отвечающая вышеприведенным требованиям для дальнейших исследований. Схема имеет управляемую камеру рабочего хода, неуправляемую камеру холостого хода с совмещенными функциями органа управления и с использованием эффекта гидравлической пружины. Данная схема отличается наименьшим количеством элементов и связей между ними, упрощающих конструкцию ударного механизма и уменьшающих число переходных процессов, обеспечивая более эффективную передачу энергии инструменту.

Ключевые слова: гидравлический ударный механизм; гидроперфоратор, структурный синтез; структурообразование; структурная формула

Introduction

Perspective of using hydraulic rock drills in the mining industry has been convincingly proven now. In this regard, it is advisable to focus on solving the issues of optimal structural and dynamic synthesis of hydraulic impact mechanisms (HIM), as the most complex and critical elements of drilling units (Yang et al., 2011; Lazutkin et al., 2015; Gorodilov et al., 2022; Chjin, 2010).

Experience in the operation of hydraulic rock drills shows that the functional reliability of the elements - the impact-piston group, the control unit, stabilizers of high and low pressure are limited. It is only 500-1000 operating hours.

In present time in the mining industry, in the construction industry, for repair of highways and the extraction of building stone, hydraulic rock drills of well-known manufacturers as Doofor (Finland), Montabert (France), Sandvik (Sweden), Everdigm (South Korea), Epiroc (Sweden), Furukawa (Japan), Soosan (South Korea), etc. are used.

Operating principle of these HIM is identical. In the basis of their construction, the main structural elements can be distinguished: a impact-piston group; the control unit; stabilizers of high and low pressure and tool (Ushakov, 2010; Mitusov, 2013; Kyzyrov et al., 2019; Yang et al., 2010). All these structural elements work in concert, but at the same time they experience high dynamic loads, are technologically difficult to manufacture due to high requirements for accuracy, tightness, quality of materials and surface hardening technology (Xu et al., 2015; Sokolski, 2017; Xu et al., 2016; Zhukov, 2023). In this regard, the issues of creating an impact mechanism that provides an effective cycle of pulsed energy conversion, low cost and manufacturability, in contrast to foreign ones with a complex control system, high requirements for manufacturing technology using expensive materials, are of particular relevance (Sokolsky, 2020; Azimov et al., 2023; Souilah et al., 2021; Yang et al., 2012).

Development of domestic manufacturing of HIM solves the problems of import substitution, increasing the technological level of domestic engineering and export orientation. For solving this problem, a scientific approach to the HIM structure formation was applied. Methods for evaluating and selecting structures for practical implementation of impact mechanisms that meet the criteria of economy, ease of constructive implementation, manufacturability and patent protection of the construction were used.

Materials and methods

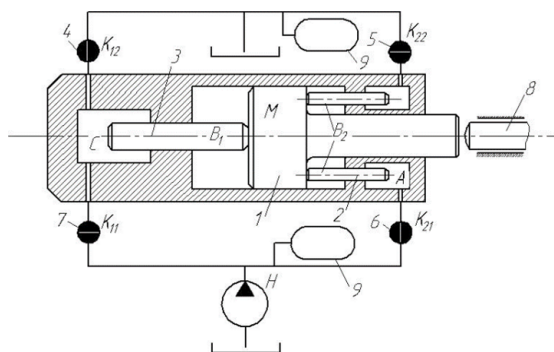
The creation of a new hydraulic impulse technic is preceded by research in the field of choosing a HIM construction scheme that meets the requirements of manufacturability and work efficiency. For choosing the constructive scheme, a structural synthesis of hydraulic impact mechanisms was used, using the main points of the method of functional structure formation, including the following steps: 1) selection of the studied object; 2) determination of its main functional purpose; 3) division of the object into structural elements; 4) obtaining structural formulas; 5) realization of formulas in constructive schemes; 6) selection of the optimal design scheme (Solod, 1968; Neroznikov, 1979).

The object of study is HIM, which is part of a hydraulic impulse system (HIS) designed to convert hydraulic energy into mechanical power impulses that carry out technological operations (drilling, crushing, etc.).

The necessary structural (functional) elements of HIM are (Figure 1):

- impact mass M (striker), perceiving a variable drive force in accordance with the phases of the working cycle, ending with the creation of a impact pulse on the tool;
- displacers B_1 and B_2 , providing a force connection between the working fluid and the impact mass M , changing the volume of fluid in chambers A and C and acting as a source of drive force;
- valves K_p , performing the functions of power supply of the working chambers and the control unit that ensures the movement of the displacers in the specified directions and sequence.

The operating principle of HIM is as follows. When the inlet valve K_{21} and outlet valve K_{12} are opened, the working fluid enters the idle chamber A, acting on the displacers B_2 . The striker moves to the left of the point of impact with the tool by the amount of the working stroke h , making an idle stroke. The movement must be impactless, economical, for a limited period of time $t_{i.st}$. When the inlet valve K_{11} and outlet valve K_{22} are opened, the working fluid enters in the working stroke chamber C, acting on the working surface of the displacer B_1 , which transmits the force to the striker that moving until it hits the tool 8. The working stroke occurs. It is an acceleration of the striker to the speed of impact with the tool v_{im} in time $t_{w.st}$ and the conversion of kinetic energy $\frac{M \cdot v_{im}^2}{2}$ into a impact impulse on the tool, sufficient for effective crushing. The output parameters of the HIM are the impact energy $A = \frac{M \cdot v_{im}^2}{2}$ and impact frequency $n = \frac{1}{T}$, where $T = t_{i.st} + t_{w.st}$ is the operating cycle time.



1 - striker; 2 - displacers B_2 ; 3 - displacer B_1 ; 4-7 - valves K_{11} , K_{12} , K_{21} , K_{22} ; 8 - tool; 9 - stabilizers of high and low pressure; H - pump

Figure 1. The structure of the hydraulic impact mechanism

The system-forming links between the functional elements of HIM are kinematic and constructive links. Kinematic link ensures the integration of functional elements into a single system to perform a given function. Conventionally, the kinematic link is denoted by the symbol (+). A constructive link allows you to combine two or more functions in one element while maintaining the system's operability and is denoted by the symbol () .

A different combination of kinematic and constructive links of functional elements leads to the formation of structural formulas that determine the structure of the impact mechanism. When certain restrictions are imposed on the combination of links between functional elements, it is possible to obtain structural formulas for various classes of impact mechanisms.

The process of obtaining structural formulas is called structure formation, as a result of which complete structures can be obtained that contain all the functional elements to ensure the working cycle and incomplete structures, in which some of the functional elements degenerate without transferring their functions to other elements (Solod, 1968; Neroznikov, 1979). The method of degeneration or substitution of functions can be realized in the following ways: 1) degeneration of elements K_{21} and K_{22} of the idle chamber control; 2) degeneration of elements K_{11} and K_{12} of the working stroke chamber; 3) combined degeneracy of elements.

Thus, using the accepted symbols of the elements and symbols of the links, it is possible to compose formulas for HIM structures that reflect the composition and nature of the links between the elements. A different combination of structural and kinematic links with elements leads to the formation of groups of valve, valveless and combined structures of impact mechanisms (Figure 2):

$$M + B_1 + B_2 + K_{11} + K_{12} + K_{21} + K_{22}; \quad (1)$$

$$M \cdot B_1 \cdot B_2 \cdot K_{11} \cdot K_{12} \cdot K_{21} \cdot K_{22}; \quad (2)$$

$$M + B_1 \cdot K_{11} \cdot K_{12} + B_2 + K_{21} + K_{22}. \quad (3)$$

Formulas (1) - (3) determine the structures of HIM schemes.

A distinctive feature of valve HIM is the absence of alignment links between the impact mass, displacers and valves. On the contrary valveless HIM is characterized by the presence of combination links between valves and other elements. A feature of combined HIM is that some of the valves are functionally combined with the impact mass and displacers, and some of them operate autonomously.

No matter of belonging to one group or another, all impact mechanisms are divided into single- and double-acting ones. In double-acting impact mechanisms both chambers communicate with a source of hydraulic energy, in single-acting mechanisms one chamber communicates.

For constructive realization and selection of the optimal structure, in the future, structure formation is considered on the example of valveless impact mechanisms or mechanisms with a combined control body as the most promising and universal HIM.

Structure formation makes it possible to obtain a number of formulas for HIM structures with a combined control body, in which the functions of the inlet and outlet valves are performed by the striker and displacers. To actuate the inlet and outlet valves of the working and idling chambers, you can use both the reciprocating movement of the striker and displacers, as well as other movements (rotary, turning, etc.). The first variant leads to the formation of autonomous mechanisms, the performance of the valves in which is provided by the system itself without additional elements. The second variant leads to the formation of mechanisms, the operation of valves in which is provided by additional elements, for example, a hydraulic motor for rotating the impact mass (Mitusov, 2013; Neroznikov, 1979; Uraimov et al., 2019).

To implement the principle of designing HIM schemes with a combined control body, it is necessary that the working and idle chambers, except the closedness and variability of the working volume have the elastic properties necessary to remember and maintain hydraulic signals for a certain time. During the operation of HIM, the working chamber must remember the hydraulic signal (pressure) when it is connected by an inlet valve to the pressure line. This chamber must accompany the movement of the striker until the next signal is given, which is possible due to the connection of the working chamber by outlet valve with the drain line. As a memory device, a hydraulic reservoir can be used, which provides additional elastic properties in the working chamber due to the compressibility of the working fluid.

The synthesis of HIM was carried out taking into account the following provisions:

1. In the working chambers only hydraulic energy is converted into mechanical work;
2. Complete structures are formed from the entire set of functional elements by composition based on kinematic, constructive and constructive-kinematic links;
3. Incomplete structures are formed from a reduced number of functional elements based on the above links;
4. The degeneration of any of the functional elements leads to the loss of system performance;
5. Substitution of degenerate functional elements is carried out only within the HIM.

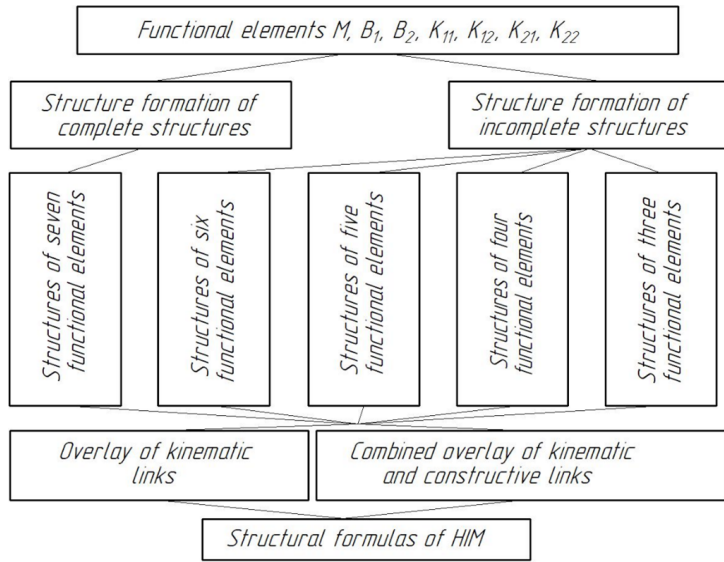
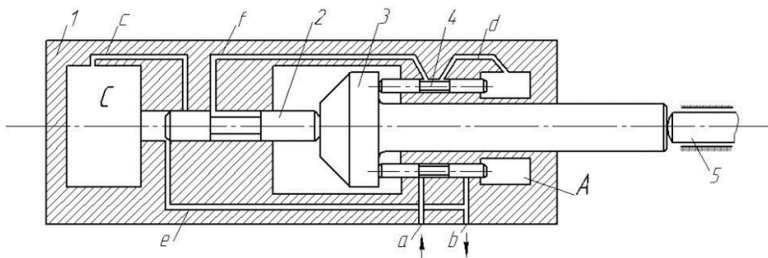


Figure 2. Scheme of HIM structure formation

Results and discussions

The constructive realization of the complete structures consists in the representation of the available elements and the distribution of the functions of the inlet valves and outlet valves between them. Figure 3 shows an example of a constructive scheme of HIM with a complete structure. The structure formula of mechanism is:

$$M + B_1 \cdot K_{11} \cdot K_{12} + B_2 \cdot K_{21} \cdot K_{22}. \quad (4)$$



A and C - chambers of idle and working strokes respectively;
1 - body; 2, 4 - displacers; 3 - striker; 5 - tool

Figure 3. Scheme of the impact mechanism with a complete structure

When fluid is supplied to chamber A, the striker 3, under the action of a force applied to the displacers 4, moves away from the tool 5 and, compressing the fluid in chamber C after the drain channel is blocked by displacer 2, makes idle stroke. At the end of idle stroke, due to the opening of the pressure channel «c» by displacer 2, chamber C communicates with the pressure line, and chamber A, due to the opening of the drain channel «b» by displacers 4, communicates with the drain line. There is a striker

deceleration. Since the pressure in chamber C is equal to the main pressure, the striker begins its working stroke. First, the striker 3 moves when the inlet channel «c» and the drain channel «b» are opened. Then they overlap and further movement of the striker is carried out due to the expansion of the volume of fluid in chamber C, while the fluid in chamber A is compressed. At the end of the working stroke, the striker 3 strikes the tool. Chamber C, due to the opening of the drain channel «e» by the displacer 2, communicates with the drain channel, and chamber A, due to the opening of the inlet channel «d» by the displacers 4, communicates with the pressure line.

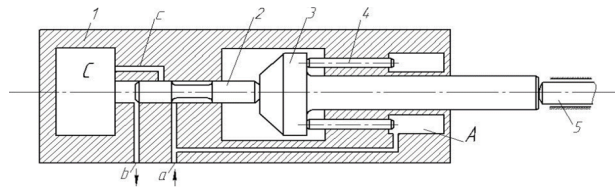
Degenerate structures are characterized by the fact that they can be deprived of one of the working chambers (when one of the displacers degenerates), as well as power control elements of one or two chambers (when one, two or three valves degenerate). The constructive implementation of degenerate structures is complicated by the fact that the degeneration of any element leads to a loss of efficiency of the constructive scheme. This is explained by the fact that the ability to control the movement of the striker is lost due to a breakdown in the connection of one or two chambers with the pressure or drain lines. With the constructive implementation of such structures, the operability of the schemes should be restored by creating new links instead the broken ones either due to the elements of the HIS subsystems or due to the elements of other external systems. The first method allows to restore the operability of impact mechanism schemes within one autonomous system without resorting to other surrounding systems for help. The second method leads to the emergence of non-autonomous (dependent) schemes, since it allows restoring the working capacity of impact mechanisms due to elements of external systems.

With the constructive implementation of formulas with degenerate elements of the control element of one of the chambers, the performance of HIM schemes is restored due to the constant connection of this chamber with the power source, i.e. with hydraulic transmission subsystem. An example of a constructive scheme with degenerate inlet and outlet valves of the idle chamber is shown in Figure 4. The formula for the structure of the mechanism is:

$$M + B_1 \cdot K_{11} \cdot K_{12} + B_2. \quad (5)$$

When fluid is supplied to chamber A, the striker 3, under the action of a pressure force constantly applied to displacers 4, moves away from tool 5. Further, compressing the fluid in chamber C, after blocking the drain channel «b» by displacer 2, striker makes idle stroke. At the end of idle stroke, due to the opening of pressure channel «c» by displacers 2, chamber C communicates with the pressure line. There is a striker deceleration.

Since the cross section of the displacer 2 is greater than the total area of the sections of the displacers 4, and the pressure acting on them is the same, the striker begins the working stroke. First, the striker 3 moves with the inlet channel «c» open, which then overlaps and the further movement of the striker 3 is carried out due to the expansion of the fluid in the chamber C. At the end of the working stroke, the striker 3 strikes the tool 5, and the chamber C, due to the opening of the drain channel «b» by the displacer 2, communicates with the drain line. Then the cycle repeats.



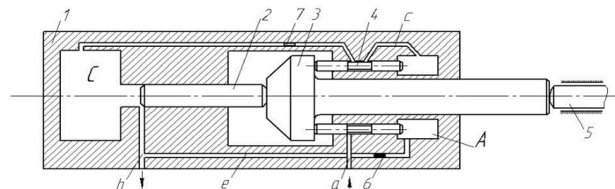
A and C - chambers of idle and working strokes respectively; 1 - body;
2, 4 - displacers; 3 - striker; 5 - tool

Figure 4. Scheme of the impact mechanism with degenerate valves K_{21} , K_{22}

With the constructive implementation of formulas with degenerate inlet valves or drain line of one or two chambers, the operability of the schemes of hydraulic impact mechanisms is restored due to the constant connection of these chambers through a separating element with a pressure or drain line. The separating element is subject to the requirements of limited inlet and outlet amount of fluid. As a separating element, a throttle with a constant flow area can be used. An example of a structural diagram with degenerate inlet and outlet valves for the working and idle chambers is shown in Figure 5. The formula for the mechanism is:

$$M + B_1 \cdot K_{12} + B_2 \cdot K_{21}. \quad (6)$$

When fluid is supplied to chamber A, the striker 3, under the action of force applied to the displacers 4, moves away from the tool 5. Further, compressing the fluid in chamber C, after blocking the drain channel «b» by displacer 2, striker makes idle stroke. At the end of idle stroke, the pressure in chamber C becomes equal to the main one due to its constant communication through the separating element 7 and channel «a» with the pressure line. In chamber A pressure is equal to value in the drain line, due to its constant communication through the separating element 6 and channels «e» and «b» with a drain line. There is a striker deceleration. Then the movement of the striker begins to the working stroke. During the working stroke, the striker moves under the action of a pressure force constantly flowing through the separating element 7 of the fluid, as well as due to its expansion in the chamber C. In this case, the fluid in the chamber A is partially compressed, and partially pushed out through the separating element 6 into the drain line. At the end of the working stroke, chamber A, due to the opening of the inlet channel «c» by displacers 4, is connected to the pressure line; chamber C due to the opening of the drain channel «b» by the displacer 2, is connected to the drain line. The striker 3 strikes the tool. Then the cycle repeats.



A and C - chambers of idle and working strokes respectively; 1 - body; 2, 4 - displacers; 3 - striker;
5 - tool; 6, 7 - separating elements (throttles)

Figure 5. Scheme of the impact mechanism with degenerate valves K_{11} , K_{22}

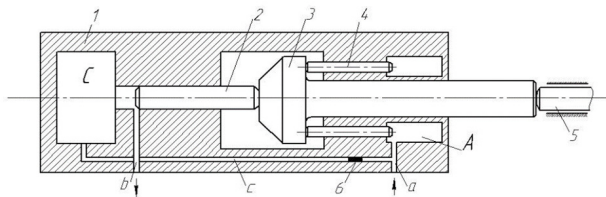
With the constructive realization of formulas with degenerate three valves, the operability of schemes of valveless hydraulic impact mechanisms is restored due to the constant connection of one of the chambers with a power source and the constant connection through the separating element of the other chamber with a pressure or drain line. An example of such constructive scheme is shown in Figure 6. The formula has the form:

$$M + B_1 \cdot K_{12} + B_2. \tag{7}$$

When fluid is supplied to chamber A, the striker 3, under the action of a pressure force constantly applied to displacers 4, moves away from tool 5 and, compressing the fluid in chamber C, after blocking the drain channel «b» by displacer 2, striker makes idle stroke. At the end of idle stroke, the pressure in chamber C becomes equal to the main one, due to its constant communication through the separating element 6 and channel «c» with the pressure line. The striker stops. Because the cross section of the displacer 2 is greater than the total area of the sections of the displacers 4, and the pressure acting on them is the same, the striker begins the working stroke. During the working stroke, the striker moves under the action of the pressure force of the fluid that constantly flowing through the separating element 6, as well as due to its expansion in the chamber C. At the end of the working stroke, chamber C, due to the opening of the drain channel «b» by displacer 2, communicates with the drain line, and the striker strikes the tool. Then the cycle repeats.

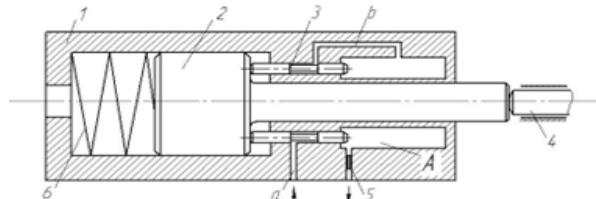
With the constructive realization of formulas with degenerate elements B_1, K_{11}, K_{12} or B_1, K_{21}, K_{22} , the operability of HIM schemes is restored by using elements of other environmental systems. An example of such constructive scheme is shown in Figure 7. The mechanism formula is:

$$M + B_2 \cdot K_{21}. \tag{8}$$



A and C - chambers of idle and working strokes respectively; 1 - body; 2, 4 - displacers; 3 - striker; 5 – tool; 6 - separating element (throttle)

Figure 6. Scheme of the impact mechanism with degenerate valves K_{21}, K_{22}



A - chamber of idle stroke; 1 - body; 2 - striker; 3 - displacers; 4 – tool; 5 - separating element (throttle); 6 - spring

Figure 7. Scheme of the impact mechanism with degenerate elements $B_1, K_{11}, K_{12}, K_{22}$

When fluid is supplied to the chamber A, the striker 2, under the action of the force applied to the displacers 3, moves away from the tool and, compressing the spring 6, makes an idle stroke. At the end of idle stroke, the pressure in the chamber A becomes equal to the drain one, due to its constant communication through the separating element 5 with the drain line. The striker stops. Because the elastic force of the spring 6 acts on the striker 2, and the pressure in the chamber A is equal to the drain pressure, the working stroke begins. During the working stroke, the fluid in the chamber A is partially compressed, and partially pushed out through the separating element 5 into the drain line. At the end of the working stroke, chamber A, due to the opening of the inlet channel «b» by displacers 3, is connected to the pressure line, the striker strikes the tool 4. Then the cycle repeats.

Due to the significant number of structural formulas and schemes resulting from constructive implementation, the analysis and study of HIM schemes becomes more complicated. Therefore, it is more expedient to determine the structures of the constructive schemes of HIM, the working process in which would be identical, and then, grouping them, to conduct research.

Thus, in order to obtain a visual representation of the constructive schemes of HIM with a combined control body, according to the number and characteristics of the combined valves, the impact mechanisms can be divided into 15 groups, the analysis of which allows us to note the following (Figure 8):

- the first group is characterized by the presence of two controlled chambers, in which the change of the working volume occurs due to compression and expansion of the fluid in them, as well as their periodic connection with the pressure and drain lines in the working process;

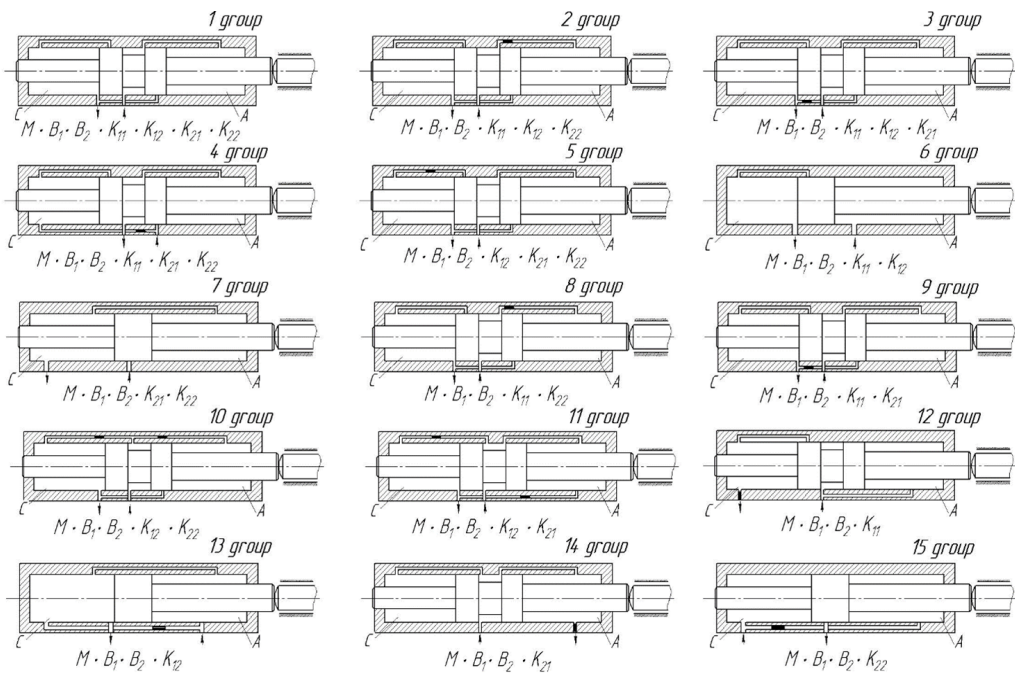
- the second group is characterized by the presence of two controlled chambers, and the idle chamber is constantly connected by a throttle to the pressure line. The working process is characterized by the absence of a periodic process of fluid inlet into the idle chamber;

- the third group is characterized by the presence of two controllable chambers and the constant connection of the idle chamber through the separating element with the drain line. The working process is characterized by the absence of a periodic process of discharging fluid from the idle chamber;

- the fourth group is characterized by the presence of two controlled chambers and the constant connection of the working stroke chamber through a separating element with a drain line. Its working cycle is characterized by the absence of a periodic process of discharging fluid from the working stroke chamber;

- the fifth group is characterized by the presence of two controlled chambers and the constant connection of the working stroke chamber through a separating element with a pressure line. In the working cycle of this group, there is no periodic process of fluid inlet into the working stroke chamber;

- the sixth group is characterized by the presence of one controlled working stroke chamber, as well as the constant connection of the idle chamber with the pressure line or its absence at all. This group is characterized by the absence of the compression and expansion processes of the fluid in the idle chamber and its periodic connection with the pressure and drain lines;



A and C - chambers of idle and working strokes, respectively

Figure 8. Schemes of HIM with a combined control body

- the seventh group is characterized by the presence of one controlled idle chamber, as well as the constant connection of the working stroke chamber with the pressure line or its absence. This group is characterized by the absence of the compression and expansion processes of the fluid in the working stroke chamber and its periodic connection with the pressure and drain lines;

- the eighth group is characterized by the presence of two controlled chambers and constant communication through the separating elements of the idle chamber with pressure line and the working stroke chamber with drain line. The working cycle is characterized by the absence of a periodic process of fluid inlet into the idle chamber and its discharging from the working stroke chamber;

- the ninth group is characterized by the presence of two controlled chambers and constant communication through the separating elements of the working and idling chambers with the drain line. There is no periodic process of discharging fluid from both chambers;

- the tenth group is characterized by the presence of two controlled chambers and constant communication through the separating elements of the working and idle chambers with the pressure line. In the working cycle of this group, there is no periodic process of fluid inlet into the idle and working stroke chambers;

- the eleventh group is characterized by the presence of two controlled chambers and constant communication through the separating elements of the working stroke chamber with pressure line and idle chamber with drain line. The schemes of this group do not

have the process of fluid inlet into the working stroke chamber and its discharging from the idle chamber;

- the twelfth group is characterized by the presence of one controlled working stroke chamber and its constant connection through a separating element with a drain line, a constant connection of the idle chamber with a pressure line or its absence. The working cycle is characterized by the absence of a periodic process of discharging fluid from the working stroke chamber, as well as the absence in the idle chamber of the process of fluid compression and expansion and its periodic connection with the pressure and drain lines;

- the thirteenth group is characterized by the presence of one controlled working stroke chamber and its constant connection through the separating element with the pressure line, the constant connection of the idle chamber with the pressure line or its absence. The working cycle is characterized by the absence of a periodic process of fluid inlet into the working stroke chamber; the absence in the idle chamber of the process of fluid compression and expansion and its periodic connection with the pressure and drain lines;

- the fourteenth group is characterized by the presence of one controlled idle chamber and its constant connection through the separating element with the drain line, as well as the constant connection of the working stroke chamber with the pressure line or its absence. The working cycle is characterized by the absence of a periodic process of discharging from the idle chamber; the absence in the working stroke chamber of the process of fluid compression and expansion and its periodic connection with the pressure and drain lines;

- the fifteenth group is characterized by the presence of one controlled idle chamber and its constant connection through the separating element with the pressure line, the constant connection of the working stroke chamber with the pressure line or its absence. The working cycle is characterized by the absence of a periodic process of fluid inlet into the idle chamber; the absence in the working stroke chamber of the process of fluid compression and expansion and its periodic connection with the pressure and drain lines.

An analysis of the features that characterize each group showed that some features are common to all groups. Such a sign is the controllability of the working chambers, according to which impact mechanisms can be:

- with two controlled chambers (1 group);
- with two controlled chambers and with separating elements in them (2,3,4,5,8,9,10,11 groups);
- with a controlled working stroke chamber (group 6);
- with a controlled working stroke chamber and with a separating element in it (12,13 groups);
- with a controlled idle chamber (group 7);
- with a controlled idle chamber and a separating element in it (14,15 groups).

When choosing for further research a group of HIM schemes in relation to drilling machines, the main factor is the perfection of the structure and the process of energy

conversion in the working chambers. Analysis of the features that characterizing the operating cycle of groups of schemes of impact mechanisms with separating elements have a direct connection of the pressure line through the working chamber and the separating element with a drain line. As a result, the working processes of the mechanisms of groups 2,3,4,5,8,9,10,11,12,13,14,15 are not economical due to the increased fluid flow due to the presence of fluid overflows through the throttles in the working cycle.

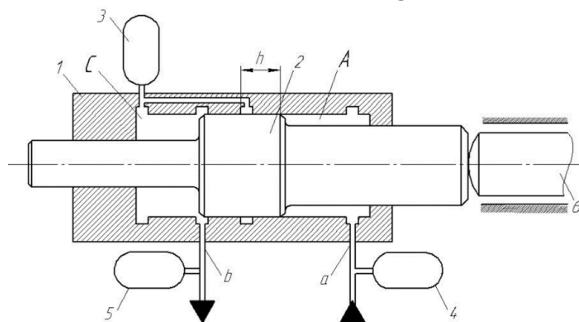
Groups 1, 6 and 7 will have a more economical energy conversion process, since they discharge fluid into the drain line after its preliminary expansion in the working chambers. From the point of view of the efficiency of the energy conversion process, groups 1, 6 and 7 are the same, however, from the point of view of structural perfection, simplicity of design, preference should be given to groups 6 and 7. The structural formulas of these groups have a smaller number of elements, and the schemes of their mechanisms contain only one controlled working chamber, equipped with an additional hydraulic capacity, which reduces the number of transients.

As a result of comparing the schemes of groups 6 and 7, it can be noted that the HIM with a controlled idle chamber cannot be recommended for constructive implementation due to a significant increase in the forces developed in the idle and working stroke chambers, on which inertial, volumetric and hydraulic losses are directly proportional and which, according to the task, should be minimal (Mitusov, 2013; Kyzyrov et al., 2019).

Conclusion

Thus, as a result of the structural analysis of HIM, the possibility of realization a simplified structural scheme with a combined control body using the effect of a hydraulic spring in the working chambers was revealed. Piston-driven working chamber A in the process of completing the working cycle is periodically connected to the high pressure hydraulic stabilizer 4 (at the end of the idle stroke) and to the low pressure hydraulic stabilizer 5 (at the end of the working stroke).

The result is a discrete increase or decrease of the energy level of the controlled working chamber. The working cycle is performed by changing the energy level of the additional volume of fluid 3 in the controlled working stroke chamber C (Figure 9).



A, C - chambers of idle and working strokes, respectively; 1 - body; 2 - piston-striker; 3 - additional volume of the working stroke chamber C; 4 - high pressure stabilizer; 5 - low pressure stabilizer; 6 - tool; a, b - pressure and drain channels, respectively; h – piston-striker stroke

Figure 9. Scheme of HIM with a combined control body

Stabilizers of high and low pressure are made in the form of calculated volumes of fluid, which also use the effect of a hydraulic spring (Raeder et al., 2021). Complex constructions of gas-fluid pressure stabilizers have been replaced by purely hydraulic stabilizers in an elastic steel shell. The structural scheme is distinguished by the smallest number of elements and connections between them, which simplifies the design of the impact mechanism and reduce the number of transients, which indicates a more efficient transfer of energy to the tool.

Thus, the structural synthesis of HIM made it possible to select the optimal constructive scheme of the impact mechanism that satisfies the requirements of the task.

REFERENCES

- Azimov A.M., Zhukov I.A. (2023). Review and analysis of existing technical solutions for impact hydraulic devices and formulation of problems for their improvement. *Transport, mining and construction engineering: science and production*, — 18:104–114. — DOI:10.26160/2658–3305–2023–18–104–114 (in Russ.).
- Chjin Ch. In. (2010). Determination of optimal structural parameters of hydraulic perforators, *Bulletin of the Far Eastern State Technical University [Vestnik Dal'nevostochnogo gosudarstvennogo tekhnicheskogo universiteta]*. — 3:130–135 (in Russ.).
- Gorodilov L.V., Kudryavtsev V.G. (2022) Hydraulic impactor control methods and charts, *Journal of Mining Science*, — 58:52–64. — DOI:10.1134/S1062739122010070 (in Eng.).
- Kyzyrov K.B., Mitusov A.A., Reshetnikova O.S. (2019). Technique for optimal design of constructive parameters of hydraulic impact mechanisms, *Monograph. Karaganda State Technical University, Kazakhstan*. — ISBN 978–601–315–882–2 (in Russ.).
- Lazutkin S.L., Lazutkina N.A. (2015). Perspective construction of hydraulic impact device, *Procedia Engineering*, —129:403–407. — DOI:10.1016/j.proeng.2015.12.132 (in Eng.).
- Mitusov A. A. (2013). Two-stroke impact hydraulic engines: Fundamentals of theory and calculation, *Monograph. St. Petersburg Polytechnic University, Russia*. — ISBN: 978–5–7422–4033–4 (in Russ.).
- Neroznikov Yu.I. (1979). Hydraulic drive of impact drilling machines. *Karaganda Polytechnic Institute, Kazakhstan* (in Russ.).
- Raeder T., Chernova A.A., Tenenev V.A. (2021). Incorporation of fluid compressibility into the calculation of the stationary mode of operation of a hydraulic device at high fluid pressures, *Russian Journal of Nonlinear Dynamics*, — 17(2):195–209. — DOI:10.20537/nd210205 (in Eng.).
- Sokolski M. (2017). Problems of reliability assessment of impact excitation systems of hydraulic hammers, *Journal of KONBiN*, — 41(1):129–150. — DOI:10.1515/jok–2017–0007 (in Eng.).
- Sokolsky M. (2020) Development trends and research problems of hydraulic hammers for mining and civil engineering. *Mining machines and earth-moving equipment*. Springer, Germany. — ISBN 978–3–030–25477–3 (in Eng.).
- Solod V.I. (1968). Structure formation of schemes and means of mechanization of the process of coal mining. *Moscow Mining Institute, Russia* (in Russ.).
- Souilah N., Zahzouh Z. (2021). Optimum energy calculation for a drill hammer-blow RH571-4W, *Journal of Fundamental and Applied Sciences*, — 13(1):151–171. — DOI:10.4314/jfas.v13i1.9 (in Eng.).
- Uraimov M., Eremyants V.E., Kvitko S.I. (2019). Mechanism of discrete rotation of hydraulic perforator tool. *IOP Conference Series: Earth and Environmental Science, Novosibirsk, Russia*. — P. 012080. — DOI:10.1088/1755–1315/262/1/012080 (in Eng.).
- Ushakov L.S. (2010). Hydraulic schemes of impact devices and executive bodies for mining, construction and road works, *Mining equipment and electromechanics [Gornoe oborudovanie i elektromekhanika]*. — 4:17–20 (in Russ.).
- Xu Z., Yang G., Wei H. and Ni S. (2015). Dynamic performance analysis of gas-liquid united hydraulic hammer, *Engineering*, — 7:499–505. — DOI: 10.4236/eng.2015.78046 (in Eng.).

Xu Z., Yang G. (2016). Modeling and simulation of hydraulic hammer for sleeve valve. *Engineering*, — 8:657–668. — DOI: 10.4236/eng.2016.89059 (in Eng.).

Yang G., Fang J. (2012). Structure parameters optimization analysis of hydraulic hammer system, *Modern Mechanical Engineering*, — 2:137–142. — DOI:10.4236/MME.2012.24018 (in Eng.).

Yang G., Gao J., Chen B. (2011). Computer simulation of controlled hydraulic impactor system, *Advanced Materials Research*, — 179–180:122–127. — DOI: 10.4028/www.scientific.net/AMR.179–180.122 (in Eng.).

Yang G., Liang C. (2010). Research on the new hydraulic impactor control system. *International Conference on Measuring Technology and Mechatronics Automation*, Changsha, China. — Pp. 207–210. — DOI: 10.1109/ICMTMA.2010.790 (in Eng.).

Zhukov I.A., Martyushev N.V., Zyukin D.A. et al. (2023). Modification of hydraulic hammers used in repair of metallurgical units, *Metallurgist*, — 66:1644–1652. — DOI: 10.1007/s11015–023–01480–w (in Eng.).

CONTENT

G.Yu. Abdugaliyeva, G.K. Daumova, B.E. Makhiyev, A. Akylkankyzy PROGNOSIS OF INJURIES AT METALLURGICAL PLANTS OF KAZZINC LLP BY MATHEMATICAL MODELING.....	8
B. Assanova, B. Orazbayev, Zh. Moldasheva, V. Makhatova, R. Tuleuova A FUZZY DECISION-MAKING METHOD FOR CONTROLLING OPERATION MODES OF A HARD-TO-FORMALISE RECTIFICATION COLUMN OF A DELAYED COKING UNIT.....	17
K.A. Battakova, A.A. Saipov GEOGRAPHICAL ASPECTS OF THE IMPACT OF TECHNOGENESIS ON THE ACCUMULATION OF HEAVY METALS IN SOILS AND POLLUTION OF SURFACE WATERS OF CENTRAL KAZAKHSTAN.....	31
M. Begentayev, M. Nurpeisova, E. Kuldiev, R. Nurlybaev, U. Bek STUDY OF THE INFLUENCE OF TECHNOLOGICAL FACTORS ON THE DENSITY AND STRENGTH OF ASH-GAS CONCRETE.....	45
A.A. Bokanova, A.A. Abdurrahmanov, B.K. Kurpenov, A.I. Kamardin, T.D. Imanbekova DEVELOPMENT OF A CORONA DISCHARGE GAS ANALYZER FOR AIR DISINFECTION.....	58
G.Zh. Bulekbayeva, O.G. Kikvidze, A.U. Tabylov, A.Z. Bukayeva, N.B. Suyeuova APPLICATION OF THE COMBINED FINISHING AND HARDENING METHOD FOR COMPLEX QUALITY PARAMETERS OF THE PARTS SURFACE LAYER.....	68
A.A. Volnenko, A.E. Leudanski, A.S. Serikov, A.N. Issayeva, D.K. Zhumadullayev CALCULATION AND IMPLEMENTATION OF A CYCLONE-VORTEX DEVICE IN CHROMIC SULPHATE PRODUCTION.....	80
N. Zhalgasuly, A.A. Ismailova, U.A. Bektibayev, T.Zh. Zhumagulov PURIFICATION OF PRODUCED WATER AFTER MINING.....	95
L. Zhiyenkulova, M. Yessenamanova, M. Jexenov, E.G. Koroleva, F. Nurbayeva ECOLOGICAL AND LIMNOLOGICAL RESEARCH OF THE SUSTAINABILITY OF THE ECOSYSTEM OF THE LAKE INDER.....	111
L.Z. Issayeva, Z.N. Ablessenova, K.S. Togizov, S.K. Assubayeva, L.V. Petrova HYDROTHERMALLY ALTERED ROCKS OF THE AKMAYA-QATPAR ORE ZONE AND THEIR REFLECTION IN GEOPHYSICAL FIELDS.....	128
Zh. Kadasheva, B. Mukhambetov, R. Abdinov, Ye. Kabiyeu, R. Meranzova STUDYING DWARFISM IN <i>KOCHIA PROSTRATA</i> GROWTH ON SALINE LANDS OF THE NORTHERN CASPIAN DESERT.....	143
B.Z. Kaliyev, B.K. Mauletbekova, T.D. Karmanov, B.A. Zhautikov, Zh.K. Tatayeva TECHNIQUE AND TECHNOLOGICAL FEATURES OF SEPARATION OF SPENT DRILLING FLUIDS INTO LIQUID AND SOLID PHASES FOR THE PURPOSE OF REUSE OF SEPARATION PRODUCTS.....	155

I.B. Kozhabaeva, A.A.Yerzhan, P.V. Boikachev, Z.D. Manbetova, A.K. Issataeva DEVELOPMENT OF A DIRECTION FINDER WITH DIRECTION DETERMINATION FOR SMALL-SIZED UNMANNED AERIAL VEHICLES.....	164
G. Madimarova, T. Nurpeissova, D. Kairatov, D. Suleimenova, Sh. Zhantyeva INSPECTION AND CARRYING OUT GNSS MONITORING OF POINTS OF THE STATE GEODETIC NETWORK IN THE TERRITORY OF KAZAKHSTAN.....	179
A.P. Permana, A. Suaib, R. Hutagalung, S.S. Eraku ANALYSIS OF THE RELATIVE AGE OF LIMESTONE AT TANJUNG KRAMAT REGION, GORONTALO CITY, INDONESIA.....	190
O.S. Reshetnikova, K.B. Kyzyrov, V.V. Yurchenko STRUCTURAL SYNTHESIS OF HYDRAULIC IMPACT MECHANISMS WITH A COMBINED CONTROL BODY.....	201
D. Ryskalieva, S. Syrlybekkyzy, S. Sagyndykova, A. Mustafina, G. Saparova DEPENDENCE OF MOBILE SULFUR ACCUMULATION IN SOILS AND HYDROGEN SULFIDE EMISSIONS ON THE TERRITORY OF ATYRAU.....	218
K.T. Saparov, Zh.R. Shakhantayeva, A.Ye. Yeginbayeva, N.Y. Yessenkeldiyev, J.A. Wendt THE SYSTEM OF TOPONYMS CHARACTERIZING THE GEOLOGICAL STRUCTURE AND MINERALS OF THE ZHAMBYL REGION.....	238
A. Togasheva, R. Bayamirova, M. Sarbopeyeva, M. Bisengaliev, V.L. Khomenko MEASURES TO PREVENT AND COMBAT COMPLICATIONS IN THE OPERATION OF HIGH-VISCOSITY OILS OF WESTERN KAZAKHSTAN.....	257
J.B. Toshov, K.T. Sherov, M.R. Sikhimbayev, B.N. Absadykov, A. Esirkepov ANALYSIS OF INTERACTION OF ROCK BREAKING TOOL WITH ROCK IN THE DRILLING PROCESS.....	271

Publication Ethics and Publication Malpractice in the journals of the National Academy of Sciences of the Republic of Kazakhstan

For information on Ethics in publishing and Ethical guidelines for journal publication see <http://www.elsevier.com/publishingethics> and <http://www.elsevier.com/journal-authors/ethics>.

Submission of an article to the National Academy of Sciences of the Republic of Kazakhstan implies that the described work has not been published previously (except in the form of an abstract or as part of a published lecture or academic thesis or as an electronic preprint, see <http://www.elsevier.com/postingpolicy>), that it is not under consideration for publication elsewhere, that its publication is approved by all authors and tacitly or explicitly by the responsible authorities where the work was carried out, and that, if accepted, it will not be published elsewhere in the same form, in English or in any other language, including electronically without the written consent of the copyright-holder. In particular, translations into English of papers already published in another language are not accepted.

No other forms of scientific misconduct are allowed, such as plagiarism, falsification, fraudulent data, incorrect interpretation of other works, incorrect citations, etc. The National Academy of Sciences of the Republic of Kazakhstan follows the Code of Conduct of the Committee on Publication Ethics (COPE), and follows the COPE Flowcharts for Resolving Cases of Suspected Misconduct (http://publicationethics.org/files/u2/New_Code.pdf). To verify originality, your article may be checked by the Cross Check originality detection service <http://www.elsevier.com/editors/plagdetect>.

The authors are obliged to participate in peer review process and be ready to provide corrections, clarifications, retractions and apologies when needed. All authors of a paper should have significantly contributed to the research.

The reviewers should provide objective judgments and should point out relevant published works which are not yet cited. Reviewed articles should be treated confidentially. The reviewers will be chosen in such a way that there is no conflict of interests with respect to the research, the authors and/or the research funders.

The editors have complete responsibility and authority to reject or accept a paper, and they will only accept a paper when reasonably certain. They will preserve anonymity of reviewers and promote publication of corrections, clarifications, retractions and apologies when needed. The acceptance of a paper automatically implies the copyright transfer to the National Academy of Sciences of the Republic of Kazakhstan.

The Editorial Board of the National Academy of Sciences of the Republic of Kazakhstan will monitor and safeguard publishing ethics.

Правила оформления статьи для публикации в журнале смотреть на сайте:

[www:nauka-nanrk.kz](http://www.nauka-nanrk.kz)

<http://www.geolog-technical.kz/index.php/en/>

ISSN 2518-170X (Online),

ISSN 2224-5278 (Print)

Подписано в печать 15.02.2024.

Формат 70x90^{1/16}. Бумага офсетная. Печать – ризограф.
18,0 п.л. Тираж 300. Заказ 1.